

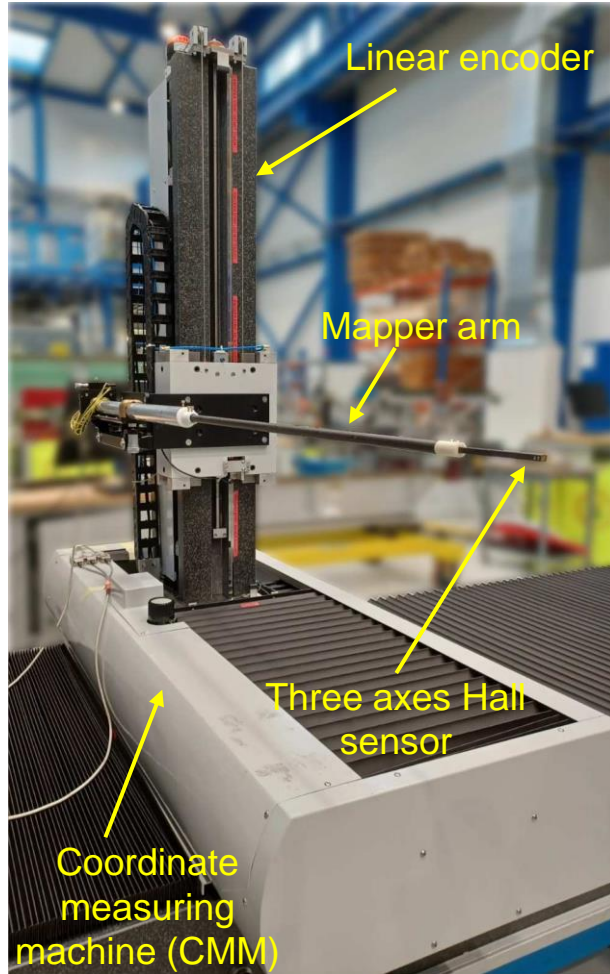
# Improving the performance of a three-axes Hall probe mapper system

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# The new Hall probe mapper system at CERN



Some machine parameters	
Measurable volume	3 x 1 x 1 m <sup>3</sup>
Resolution of the linear encoders	0.1 μm
Specified/validated positioning accuracy	0.1 mm
Maximum encoder trigger frequency	100 Hz
Nominal speed	20 mm/s

Some sensor parameters (currently equipped)	
Hall probe type	AS-3DC
Manufacturer	Projekt Elektronik
Sensor non-linearity error (calibrated)	< 0.01 % ( $ \mathbf{B}  < 1 \text{ T}$ )
Sensitivity	5 V/T
Hall sensor temperature coefficient	-0.411 mV/K
Diameter of Hall cube	2.2 mm
Sensor outer diameter	120 x 6 x 6 mm <sup>3</sup>

Some features
Precision alignment for sag correction
Precision alignment for rotation around arm axis
Keysight 3458A Digital multimeters (8.5 digit) for Hall voltages
Measurements "on-the-fly"

# Agenda

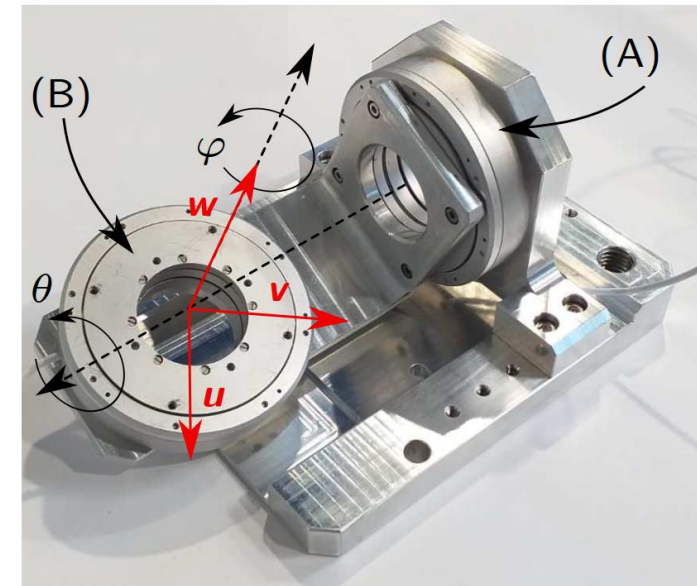
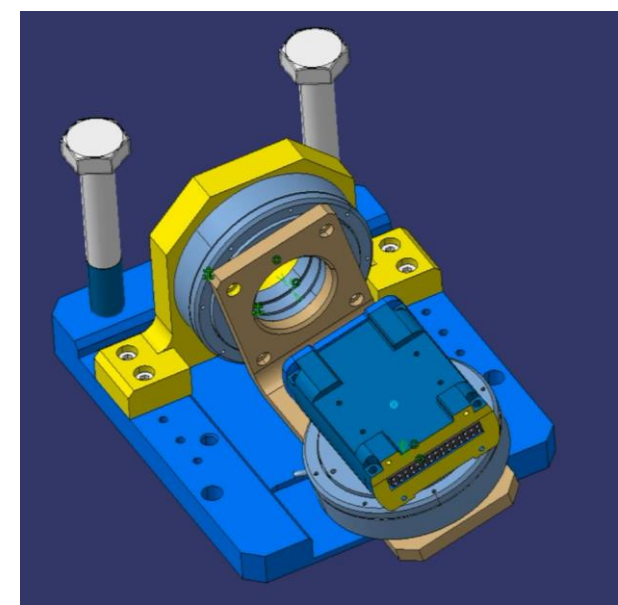
1. Sensor calibration
2. Fiducialization and alignment
3. Arm vibrations
4. Post processing
5. Outlook

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# Sensor calibration

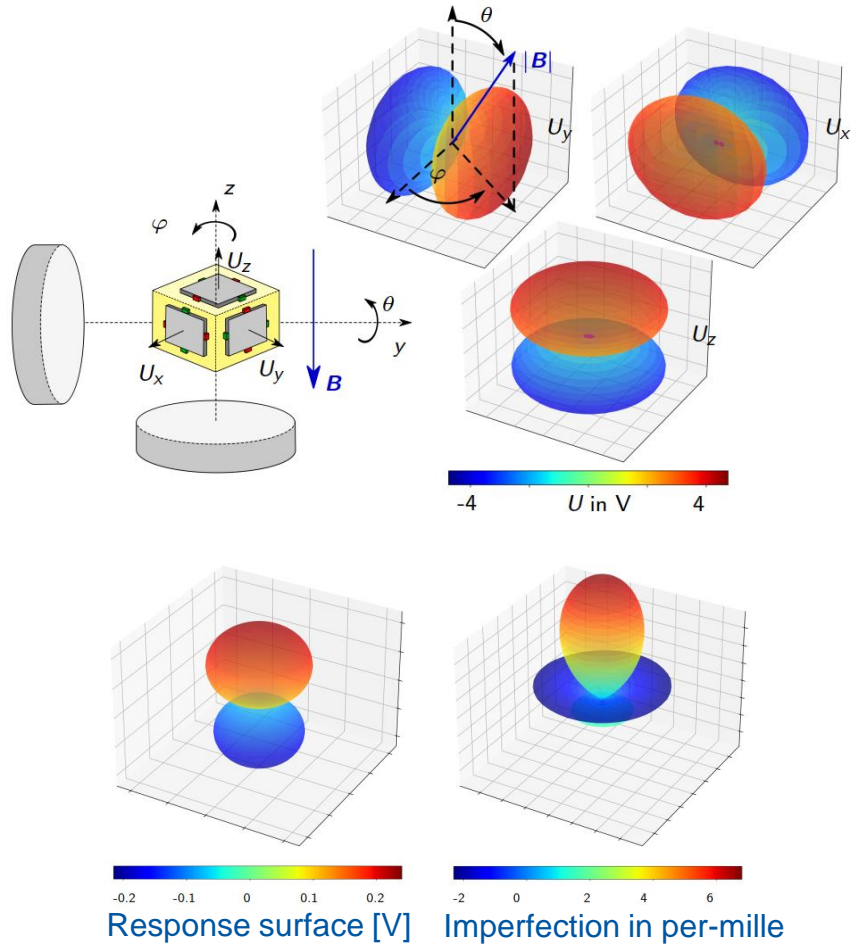
- The calibration of three axes Hall sensors is elaborate
- The new setup is designed for the calibration of
  - Non-linearity
  - Cross sensitivity (Orthogonality)
  - Planar Hall effects
- Two piezo-electric, non-magnetic rotary stages are used [1]
- Rotary encoder sensor accuracy is 25  $\mu\text{rad}$
- The assembly fits into a reference dipole of 80 mm gap height



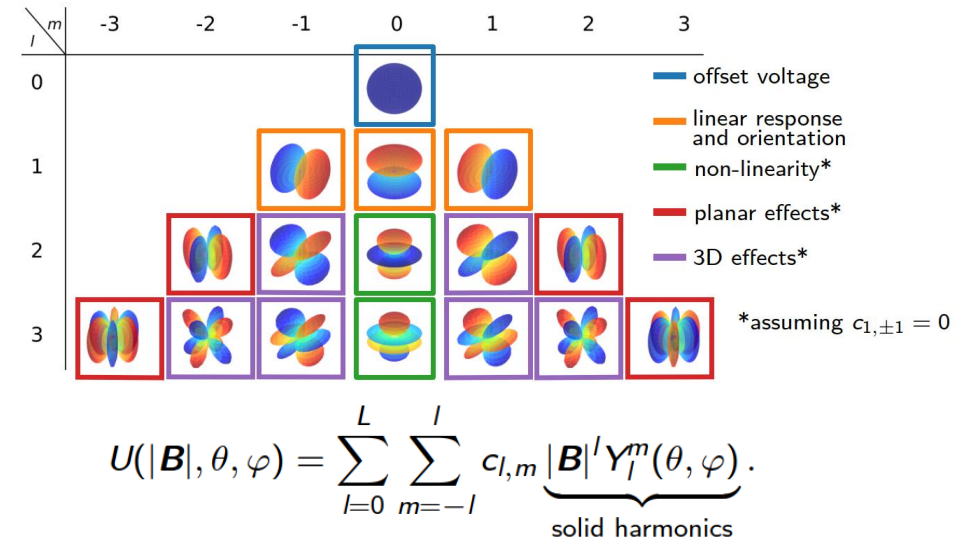
*\*Designed and manufactured by Olaf Dunkel (TE-MS-C-TM)*

# Sensor calibration

## Sensor response surfaces for a full rotation



The response surfaces can be expanded using the *solid harmonic functions* [2]



The sensor orientation is encoded in the coefficients with  $l = 1$

$$\varphi_{\max} = -\arg(c_{1,1}), \quad \theta_{\max} = \arg\left(c_{1,0} + j\sqrt{2}|c_{1,1}|\right).$$

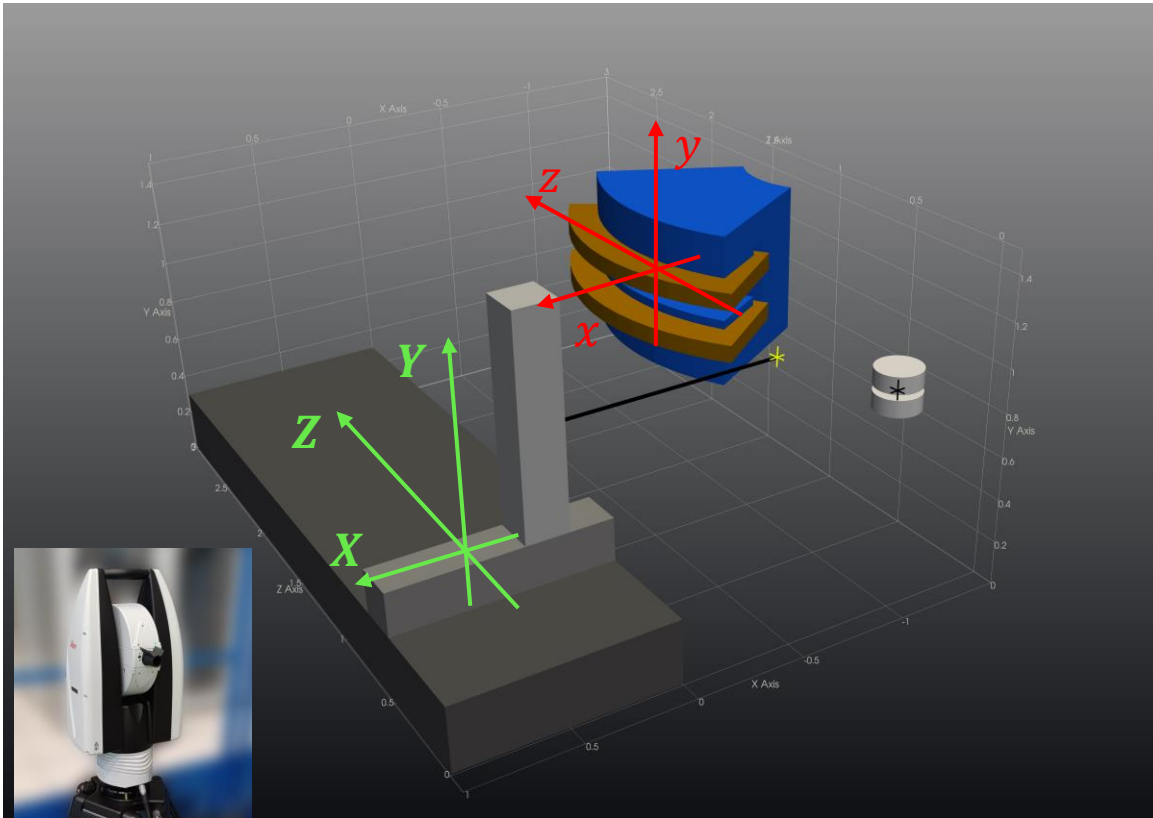
Higher order coefficients ( $l > 1$ ) provide evidence for:

- Non-linearity
- Planar and 3D Hall effects

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# Fiducialization and alignment

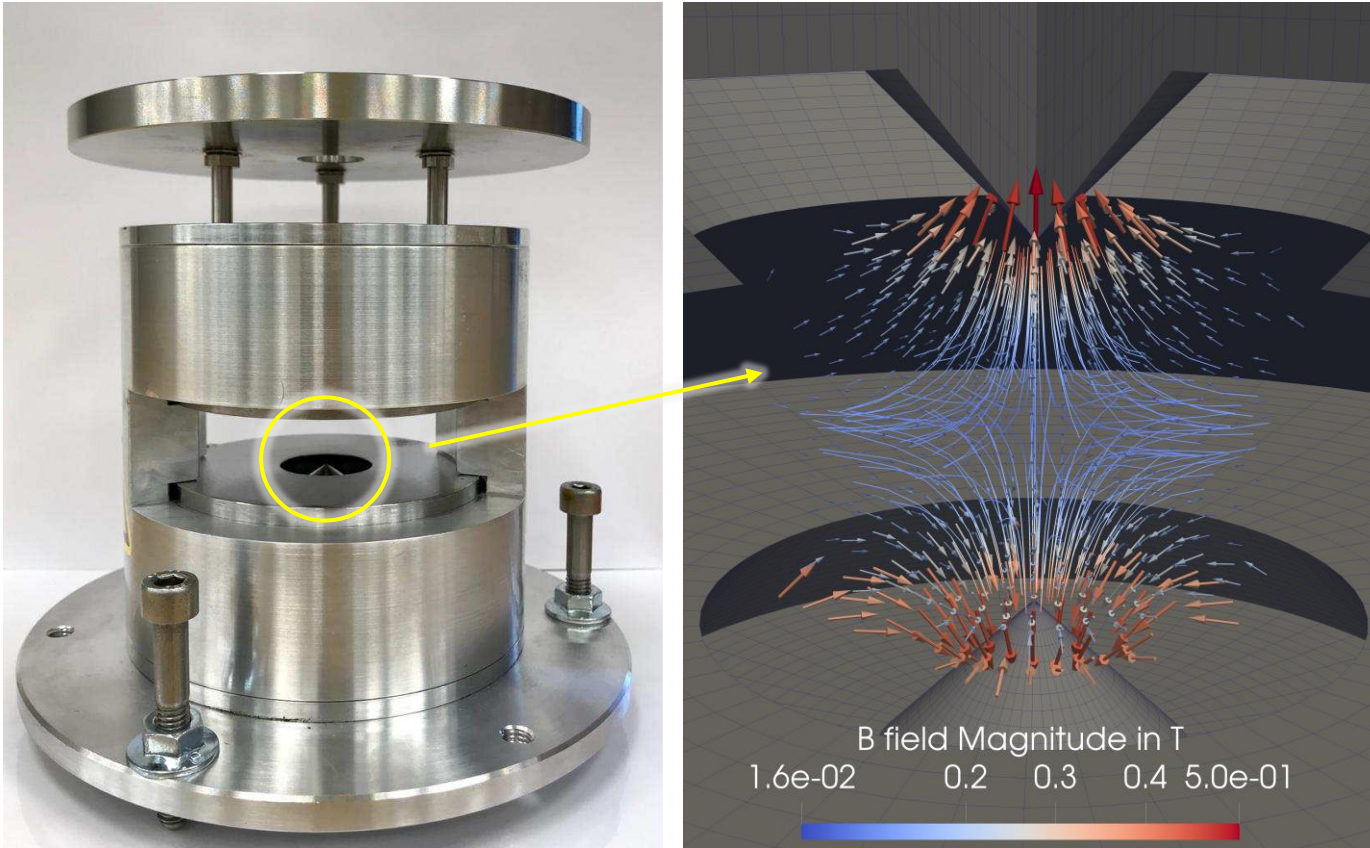


Leica AT960 [3]

- (1) A **magnet coordinate system** is constructed from optical measurements of the magnet geometry.
- (2) The **mapper orientation** vectors  $X, Y$  and  $Z$  are determined by measuring the stage movement along the three axes.
- (3) The **origin of the mapper coordinates**  $(x_0, y_0, z_0)^T$  can now be determined if the mapper coordinates are known for any point in the magnet coordinates.

$$\underbrace{\begin{pmatrix} x \\ y \\ z \end{pmatrix}}_{\text{magnet coordinates}} = \underbrace{\begin{pmatrix} X^T \\ Y^T \\ Z^T \end{pmatrix}}_{\text{mapper orientation}} \cdot \underbrace{\begin{pmatrix} X \\ Y \\ Z \end{pmatrix}}_{\text{mapper coordinates}} + \underbrace{\begin{pmatrix} x_0 \\ y_0 \\ z_0 \end{pmatrix}}_{\text{origin of the mapper coordinates}}$$

# Fiducialization and alignment

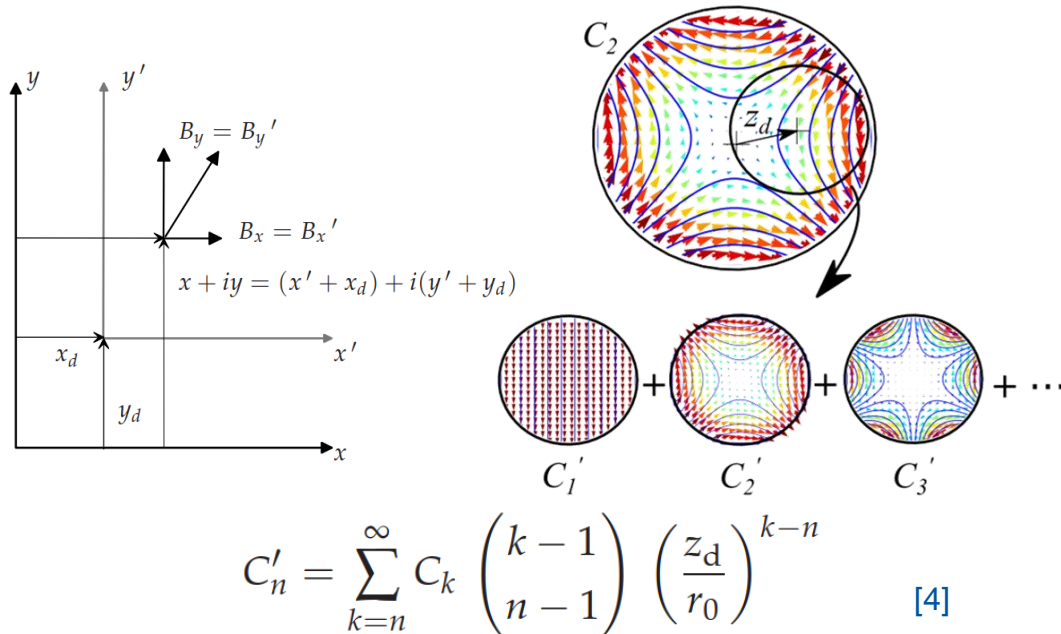


- Two permanent magnets and a yoke of electrical steel are used to shape a **rotationally symmetric  $B$ -field**
- The ***field is vanishing in the center*** of the magnet
- This ***central position is identifiable*** from the positions of three fiducialization targets on the top of the magnet
- The magnet center can be measured ***optically and magnetically***.
- In this way we can identify the ***origin of the mapper coordinates***.

*\*Designed and manufactured by Olaf Dunkel (TE-MS-C-TM)*

# Fiducialization and alignment

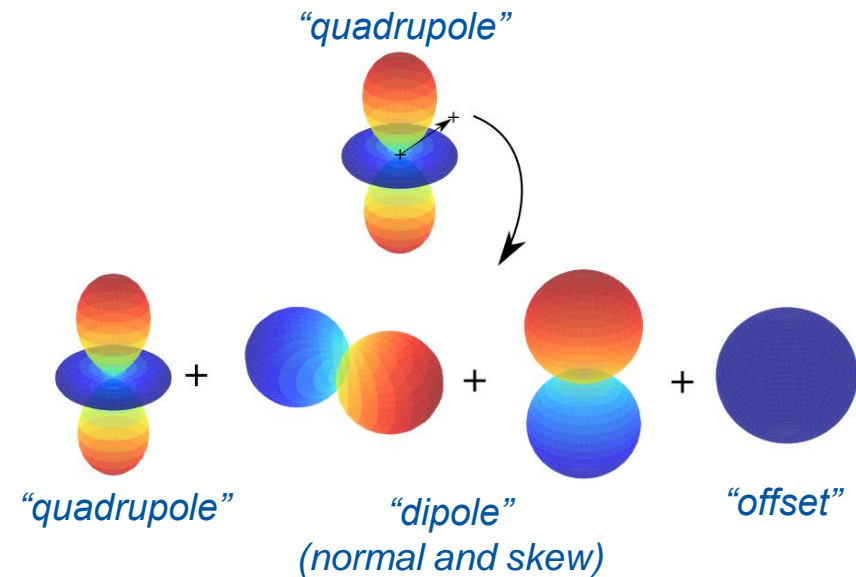
**Remember:** Feed-down correction in rotating coil measurements



Implying  $C_1 = 0$ , the sensor position  $z_d$  can be determined.

**In the 3D case:** The solid-harmonic expansion

$$\phi_m(r, \varphi, \theta) = \sum_{l=1}^{\infty} \sum_{m=-l}^l \nu_{l,m} \underbrace{r^l Y_{l,m}(\theta, \varphi)}_{\text{solid harmonics}}$$

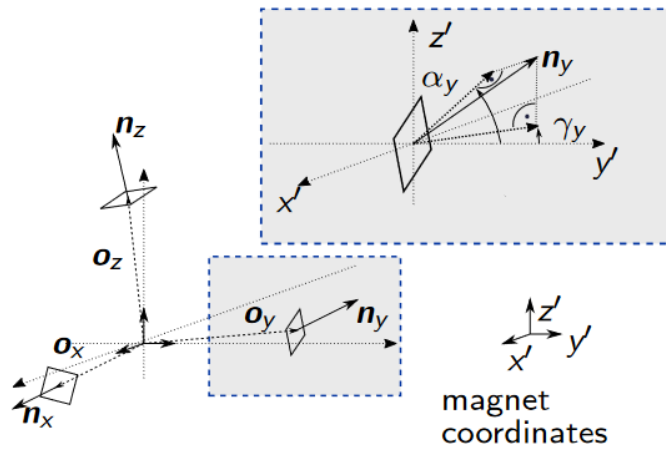


**The same principle can be applied to identify the position of the Hall sensors in the cone magnet!**

# Fiducialization and alignment

In this way we can determine:

- Absolute sensor orientation (6 DoFs)
- Absolute sensor position (9 DoFs)



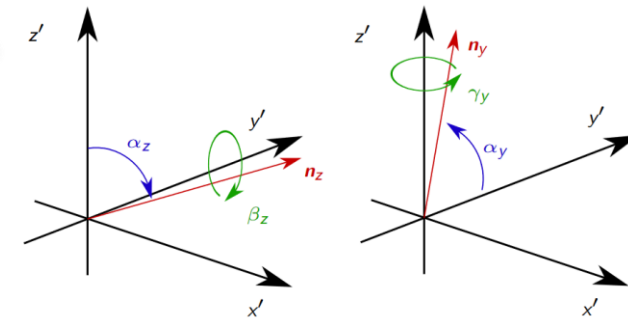
rotation around parallel axis

variable	mean <sup>1</sup>	design <sup>1</sup>	$\sigma^1$
$\alpha_y$	87.20	90	0.032
$\alpha_z$	-92.25	-90	0.025
$\beta_x$	0.79	0	0.017
$\beta_z$	75.44	0	0.456
$\gamma_x$	178.70	180	0.030
$\gamma_y$	-3.17	0	1.015

variable	mean <sup>2</sup>	design <sup>2</sup>	$\sigma^2$
$o_x$	2.08	2	0.002
$o_y$	0.05	0	0.050
$o_z$	0.01	0	0.020
$o_{xx}$	0.05	0	0.019
$o_{yy}$	0.04	0	0.017
$o_{zz}$	-2.09	-2	0.001
$o_{xy}$	0.29	0	0.050
$o_{yz}$	0.28	0.2	0.003
$o_{zx}$	-0.25	0	0.023

<sup>1</sup> values given in deg.  
<sup>2</sup> values given in mm.



orientation

position

magnets symmetry axis

The code is available in github [5]!



# Agenda

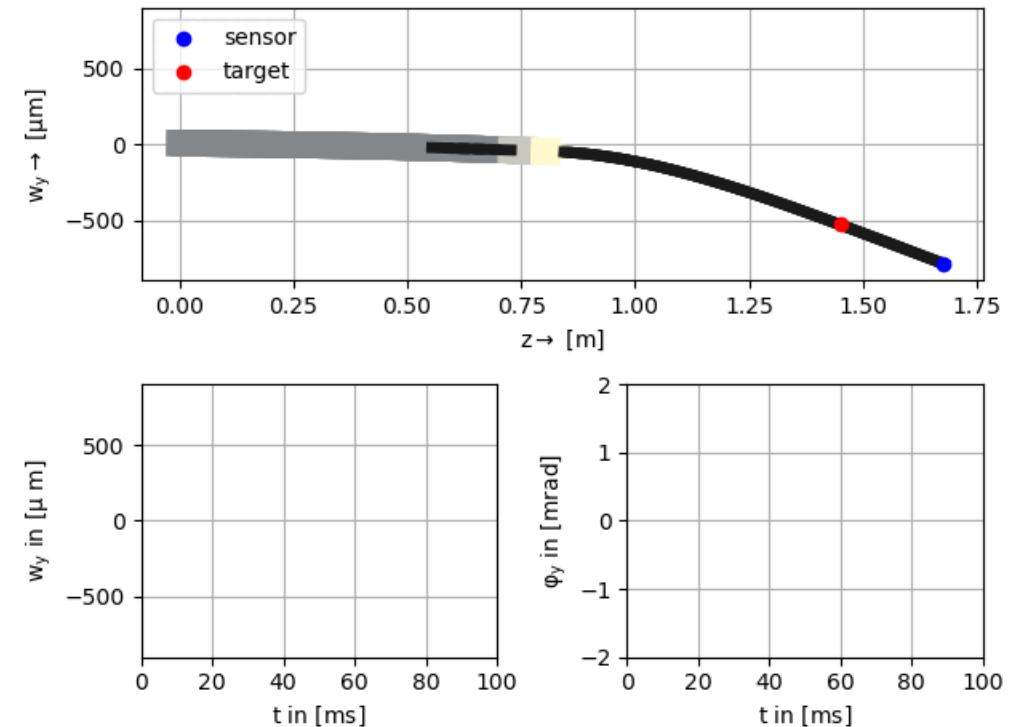
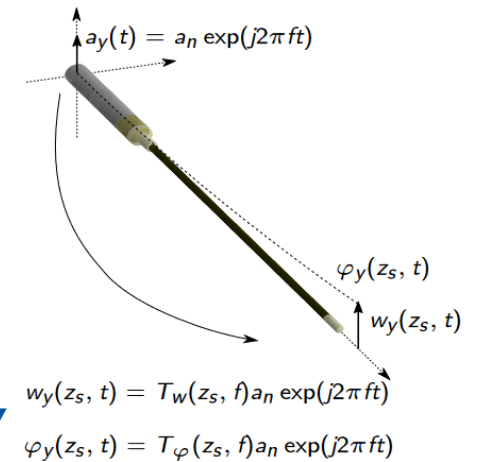
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# Arm vibrations

- Imperfections in the stage motion cause the *mapper arm to vibrate*
- We have developed a FEM model of the mapper arm using *Euler-Bernoulli beam theory*
- *The Code is available in github! [6]*

What do we get from this?

- *“Cheap” modal analysis*: Recover the vibration amplitudes and arm deformation at the sensor position from Leica measurements
- Improving the *mapper arm design*.
- Develop a *realistic noise model* including the effect of arm vibration



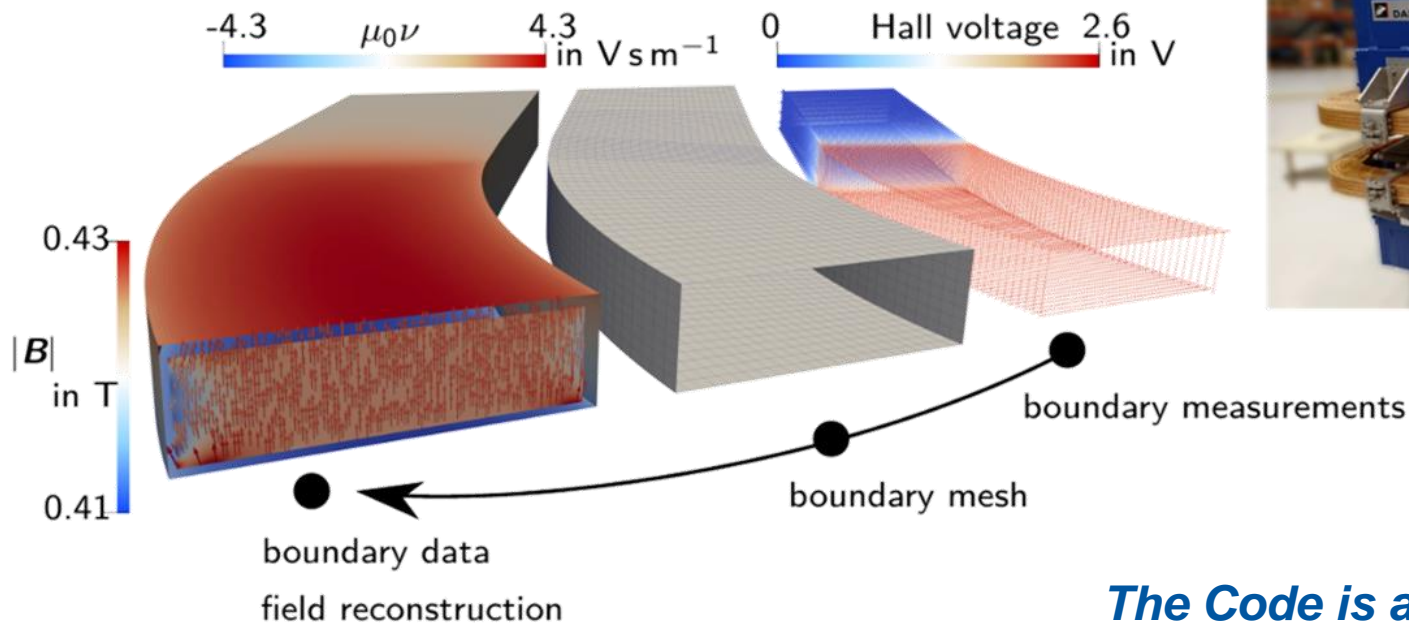
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# Post Processing

- Mapping the field along a **domain boundary** we acquire the boundary condition of a **boundary value problem**.
- We make use of **Kirchhoffs integral equation** to reconstruct the field in the enclosed domain

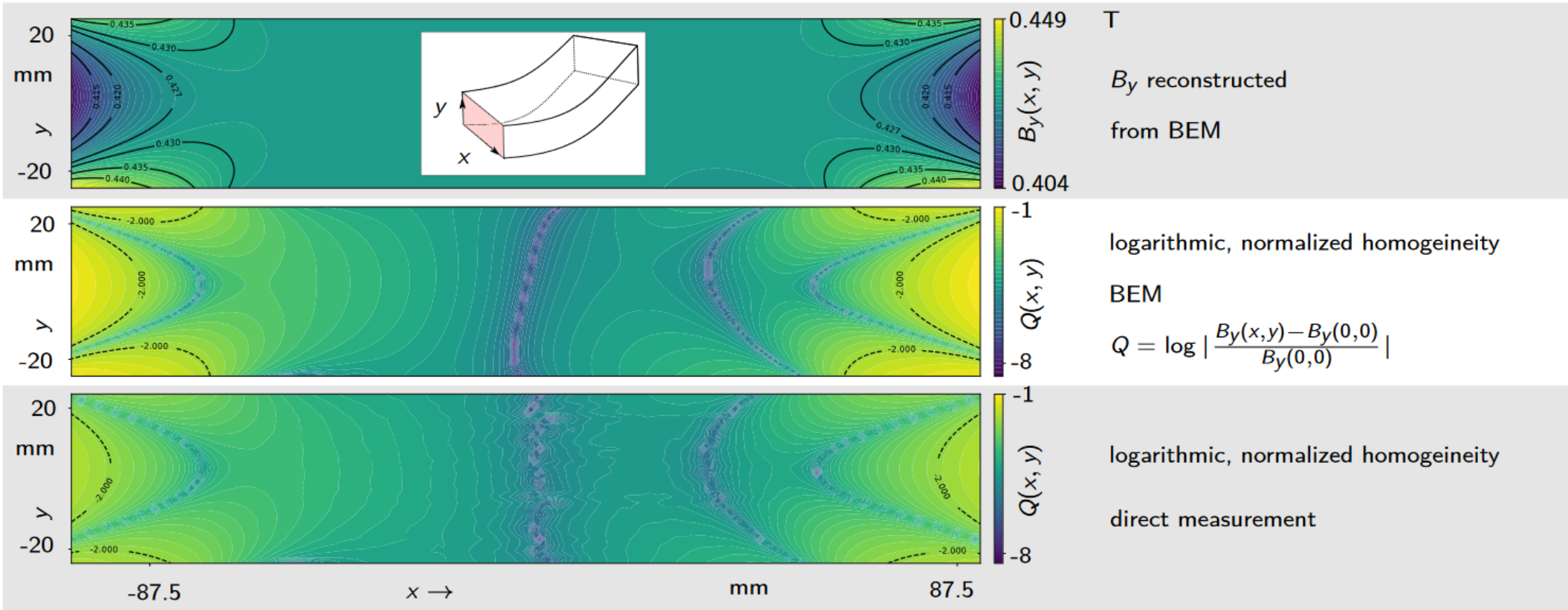
$$\underbrace{\phi_m(\mathbf{r})}_{\text{reconstructed}} = \int_{\partial\Omega} \frac{1}{4\pi|\mathbf{r} - \mathbf{r}'|} \underbrace{\frac{\partial_n \phi_m(\mathbf{r}')}{\mu_0\nu}}_{\text{measured}} d\mathbf{r}' - \int_{\partial\Omega} \underbrace{\phi_m(\mathbf{r}')}_{\text{reconstructed}} \partial_n \frac{1}{4\pi|\mathbf{r} - \mathbf{r}'|} d\mathbf{r}', \quad \mathbf{r} \in \Omega$$



**The Code is available in github! [7]**

# Post Processing

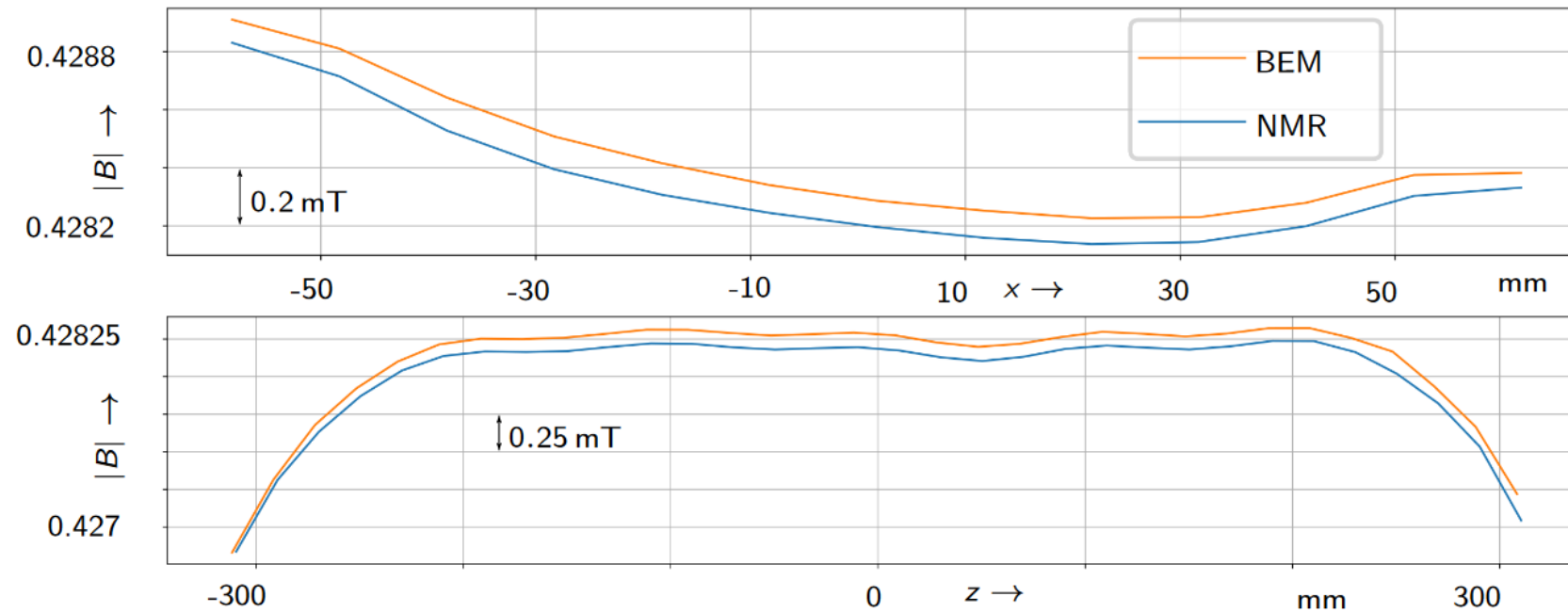
## Example



***No measurements inside the domain are needed!***

# Post Processing

## Validation by NMR measurements



A **systematic difference of 2 units** in 10 000 was found

The **temperature dependency** of the Hall voltage affects the measurements in this range

# Agenda

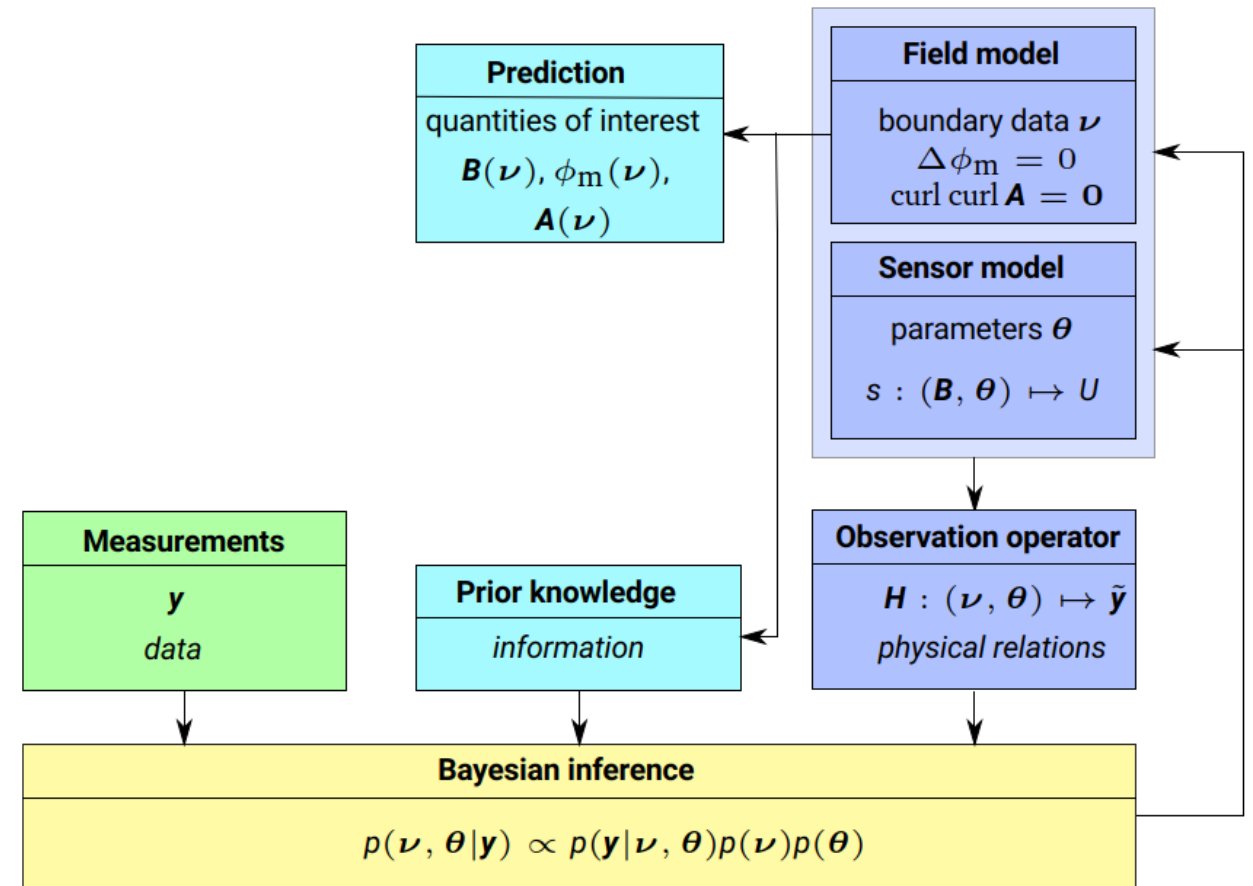
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# Outlook

## Advantages:

- **Implying Maxwells equations in the field reconstruction**
- **Non-linear and complicated sensor models are handled without approximation**
- **Multiphysical sensor modelling: Examples: Uncertain sensor **position**, sensor **temperature**, **velocity****
- **Realistic noise modelling from the coupling of the physical parameters**

## Model based field reconstruction



See [8], [9].

[8] S. Kurz, M. Liebsch et al. "Hybrid modeling: towards the next level of scientific computing in engineering".

In: (Mar. 2022). DOI: 10.1186/s13362-022-00123-0.

[9] M. Liebsch, "Inference of Boundary Data from Magnetic Measurements of Accelerator Magnets",

<https://tuprints.ulb.tu-darmstadt.de/21144/>

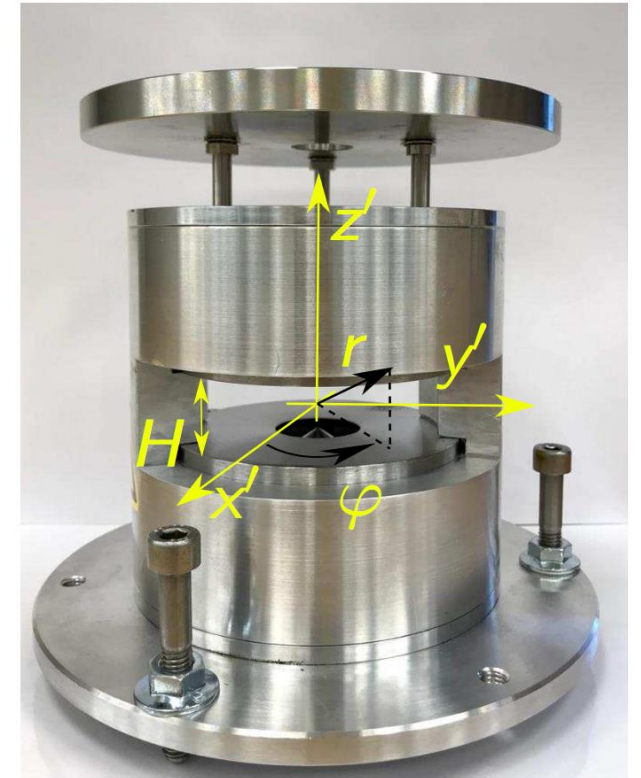
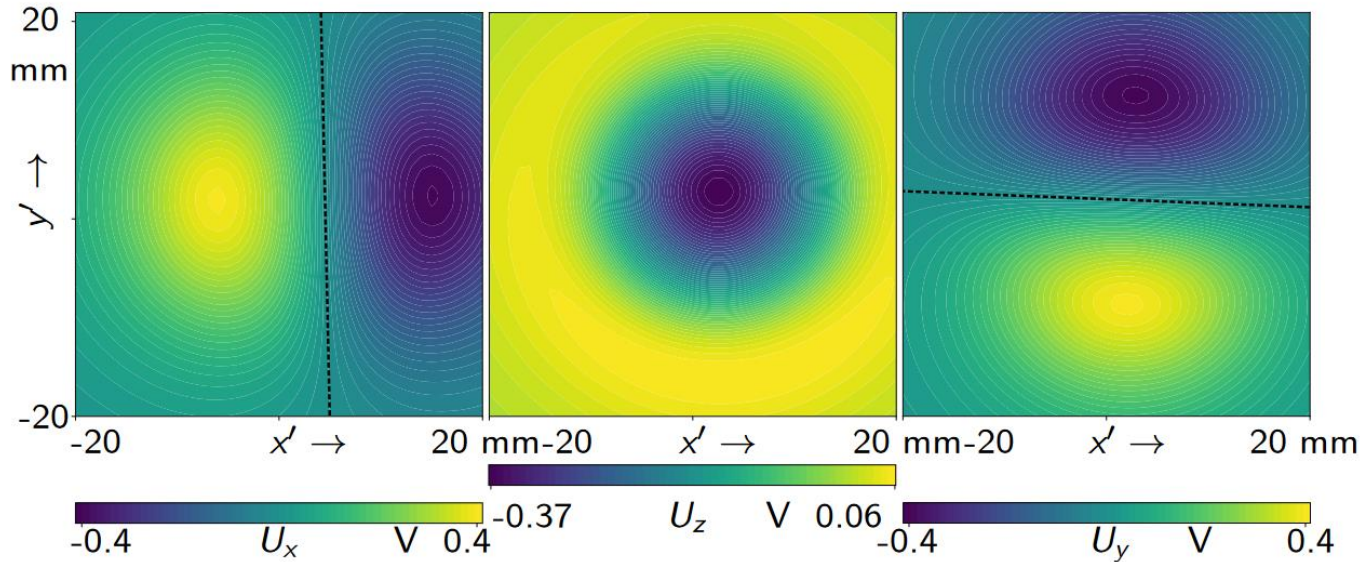
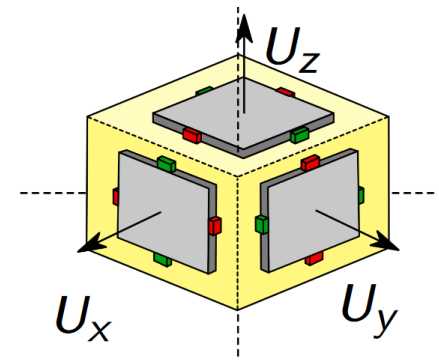
***Thank You for Your attention!***

# Backup slides

# Fiducialization and alignment

**Problem:** The three Hall probes do not really measure the three components of the vector  $\mathbf{B}$ !

**In fact:** We measure three Hall voltages related to  $\mathbf{n} \cdot \mathbf{B}$  at three different positions!



**The Hall voltages are zero along three “zero-planes” where  $\mathbf{n} \cdot \mathbf{B} = 0$ .**

**We cannot uniquely identify the positions of the Hall sensors on the zero planes!**